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INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

(51) International Patent Classification 6 : <b>F16L 11/08, 11/127</b>		<b>A1</b>	(11) International Publication Number: <b>WO 97/12166</b>
			(43) International Publication Date: <b>3 April 1997 (03.04.97)</b>
(21) International Application Number: <b>PCT/US96/15625</b>		(81) Designated States: CA, GB, JP, NO, European patent (AT, BE, CH, DE, DK, ES, FI, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE).	
(22) International Filing Date: <b>27 September 1996 (27.09.96)</b>		Published <i>With international search report.</i>	
(30) Priority Data: <b>60/004,452 28 September 1995 (28.09.95) US</b>			
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(54) Title: COMPOSITE SPOOLABLE TUBE			
(57) Abstract			
<p>A spoolable composite tube (10) capable of being spooled onto a reel for storage and for use in oil field applications. The spoolable tube exhibits unique anisotropic characteristics that provide improved burst and collapse pressures, increased tensile strength, compression strength, and load carrying capacity, while still remaining sufficiently bendable to be spooled onto a reel in an open bore configuration. The spoolable composite tube can include an inner liner (12), an interface layer, fiber composite layers, a pressure barrier layer, and an outer protective layer. The fiber composite layers can have a unique triaxial braid structure.</p>			

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## COMPOSITE SPOOLABLE TUBE

### Field of the Invention

The present invention relates generally to spoolable tubing suitable for use  
5 in the oil industry, and more particularly to spoolable tubing consisting of a composite  
material with the ability to withstand high stress.

### Background of the Invention

Spoolable tubing, that is tubing capable of being spooled upon a reel, is  
10 commonly used in numerous oil well operations. Typical oil well operations include  
running wire line cable down hole with well tools, working over wells by delivering  
various chemicals down hole, and performing operations on the interior surface of the drill  
hole. The tubes used are required to be spoolable so that the tube can be used in  
conjunction with one well and then transported on a reel to another well location. Steel  
15 coiled tubing is typically capable of being spooled because the steel used in the product  
exhibits high ductility (i.e. the ability to plastically deform). Unfortunately, the repeated  
spooling and use of steel coiled tubing causes fatigue damage that can suddenly cause the  
steel coiled tubing to fracture and fail. The hazards of operating steel coiled tubing, i.e. risk  
to personnel and high economic cost resulting from down time needed to retrieve the  
20 broken tubing sections, forces steel coiled tubing to be retired after a relatively few number  
of trips into a well.

Steel coiled tubing has also proven to be subject to expansion after repeated  
uses. Tube expansion results in reduced wall thickness with the associated reduction in the  
pressure carrying capability of the steel coiled tubing. Steel coiled tubing known in the art  
25 is typically limited to an internal pressure up to about 5,000 psi. Accordingly, higher  
pressure and continuous flexing typically reduces the steel tube's integrity and service life.

For example, the present accepted industry standard for steel coiled tube is  
an A-606 type 4 modified HSLA steel with yield strengths ranging from 70 ksi to 80 ksi.  
The HSLA steel tubing typically undergoes bending, during the deployment and retrieval of  
30 the tubing, over radii significantly less than the minimum bending radii needed for the  
material to remain in an elastic state. The repeated bending of steel coiled tubing into and  
out of plastic deformation induces irreparable damage to the steel tube body leading to low-  
cycle fatigue failure.

Additionally, when steel coiled tubing is exposed to high internal pressures  
35 and bending loads, the isotropic steel is subjected to high triaxial stresses imposed by the  
added pressure and bending loads. The high triaxial stresses result in significant plastic  
deformation of the tube and diametral growth of the tube body, commonly referred to as  
"ballooning". When the steel coiled tube experiences ballooning, the average wall

thickness of the tube is reduced, and often causes a bursting of the steel tube in the area of decreased thickness.

Steel coiled tubes also experience thinning of the tube walls due to the corrosive effect of materials used in the process of working over the well and due to materials located on the inner surface of the well bore. The thinning resulting from corrosive effects of various materials causes a decrease in the pressure and the tensile load rating of the steel coiled tubing.

It is, therefore, desirable to provide a non-steel coil tubing which is capable of being deployed and spooled under borehole conditions, which does not suffer from the limitations of steel tubing and is highly resistant to chemicals.

For the most part, prior art non-metallic tubular structures that are designed for being spooled and also for transporting fluids, are made as a hose whether or not they are called a hose. An example of such a hose is the Feucht structure in U.S. Patent 3,856,052 which has longitudinal reinforcement in the side walls to permit a flexible hose to collapse preferentially in one plane. However, the structure is a classic hose with vulcanized polyester cord plies which are not capable of carrying compression loads or high external pressure loads. Hoses typically use an elastomer such as rubber to hold fiber together but do not use a high modulus plastic binder such as epoxy. Hoses are designed to bend and carry internal pressure but are not normally subjected to external pressure or high axial compression or tension loads.

When the ends of a hose are subjected to opposing forces, the hose is said to be under tension. The tensile stress at any particular cross-section of the hose is defined as the ratio of the force exerted on that section by opposing forces to the cross-sectional area of the hose. The stress is called a tensile stress, meaning that each portion pulls on the other.

With further reference to a hose subjected to opposing forces, the term strain refers to the relative change in dimensions or shape of the hose that is subjected to stress. For instance, when a hose is subjected to opposing forces, a hose whose natural length is  $L_0$  will elongate to a length  $L_1 = L_0 + \Delta L$ , where  $\Delta L$  is the change in the length of the hose caused by opposing forces. The tensile strain of the hose is then defined as the ratio of  $\Delta L$  to  $L_0$ , i.e. the ratio of the increase in length to the natural length.

The stress required to produce a given strain depends on the nature of the material under stress. The ratio of stress to strain, or the stress per unit strain, is called an elastic modulus. The larger the elastic modulus, the greater the stress needed for a given strain.

For an elastomeric type material, such as used in hoses, the elongation at break is so high (typically greater than 400 percent) and the stress-strain response so highly nonlinear; it is common practice to define a modulus corresponding to a specified elongation. The modulus for an elastomeric material corresponding to 200 percent

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elongation typically ranges from 300 psi to 2000 psi. In comparison, the modulus of elasticity for typical plastic matrix material used in a composite tube is from 100,000 psi to 500,000 psi or greater, with representative strains to failure of from 2 percent to 10 percent. This large difference in modulus and strain to failure between rubber and plastics and thus  
5 between hoses and composite tubes is what permits a hose to be easily collapsed to an essentially flat condition under relatively low external pressure. This large difference also eliminates the hose's capability to carry high axial tension or compression loads while the higher modulus characteristic of the plastic matrix material used in a composite tube is sufficiently stiff to transfer loads into the fibers and thus resist high external pressure and  
10 axial tension and compression without collapse.

The procedure to construct a composite tube to resist high external pressure and compressive loads involves using complex composite mechanics engineering principles to ensure that the tube has sufficient strength. It has not been previously considered feasible to build a truly composite tube capable of being bent to a relatively small diameter,  
15 and be capable of carrying internal pressure and high tension and compression loads in combination with high external pressure requirements. Specifically a hose will not sustain high compression and external pressure loads.

Accordingly, it is one object of this invention to provide an apparatus and method for providing a substantially non-ferrous spoolable tube that does not suffer from  
20 the structural limitations of steel tubing and that is capable of being deployed and spooled under bore hole conditions.

A further object of the invention is to provide a composite coiled tube capable of working over wells and delivering various chemicals down hole quickly and inexpensively.

Another object of the invention includes providing a coiled tubing capable  
25 of repeated spooling and bending without suffering fatigue sufficient to cause fracturing and failing of the coiled tube.

Other objects of the invention include providing a spoolable tube capable of carrying corrosive fluids without causing corrosion in the spoolable tube, providing a coiled  
30 tube having less weight, and providing a coiled tube capable of withstanding higher internal pressure levels and higher external pressure levels without losing tube integrity.

These and other objects will be apparent from the description that follows.

#### General Description of the Invention

The invention attains the foregoing objects by providing a composite coiled tube that offers the potential to exceed the performance limitations of isotropic metals currently used in forming coiled tubes, thereby increasing the service life of the coiled tube and extending the operational parameters of the coiled tube. The composite coiled tube of  
35 the invention overcomes the disadvantages in present steel coil tubing by providing, among

other things, a composite layer that exhibits unique anisotropic characteristics capable of providing improved burst and collapse pressures as well as improved tensile strength, compression load strength, and load carrying capability.

The composite coiled tube of the present invention comprises a composite 5 layer having fibers embedded in a matrix and an inner liner formed from polymeric materials. The fibers in the composite layer are oriented to resist internal and external pressure and provide low bending stiffness. The composite coiled tube offers the potential to exceed the performance limitations of isotropic metals, thereby increasing the service life of the tube and extending operational parameters. In addition, the fibers, the matrix, and 10 the liner used in the composite coiled tube can make the tube impervious to corrosion and resistant to chemicals used in treatment of oil and gas wells or in flowlines.

The service life potential of the composite coiled tube constructed in accordance with the invention is substantially longer than that of conventional steel tube when subjected to multiple plastic deformation bending cycles with high internal pressures. 15 Composite coiled tube also provides the ability to extend the vertical and horizontal reach of existing concentric well services. In one operation, the composite coiled tube is deployed as a continuous string of small diameter tubing into a well bore to perform a specific well bore procedure. When the service is completed, the small diameter tubing is retrieved from the well bore and spooled onto a large reel for transport to and from work 20 locations. Additional applications of coiled composite tube are for drilling wells, flowlines, as well as for servicing extended reach applications such as remedial work in wells or flowlines.

In particular, the invention provides for a composite coiled tube having an inner liner formed of polymeric materials and a composite layer enclosing the inner liner. 25 The composite layer contains three fibers oriented in a triaxial braid. A triaxial braid structure is formed of three or more fibers braided in a particular orientation and embedded in a plastic matrix. In a triaxial braid, a first structural fiber helically or axially extends along the longitudinal axis of the tube. A second braiding fiber is clockwise helically oriented relative to the first structural fiber or relative to the longitudinal axis of the tube. A 30 third braiding fiber is counter-clockwise helically oriented relative to the first structural fiber or relative to the longitudinal axis of the tube. In addition, the first structural fiber is interwoven with either the second or the third or both braiding fibers. The composite coiled tube constructed with this triaxial braid structure exhibits unique anisotropic characteristics having enhanced burst pressure characteristics, collapse pressure characteristics, increased bending characteristics, tensile loads, and compression loads. 35

The composite layer can be constructed with a matrix material having a tensile modulus of at least 100,000 psi, a maximum tensile elongation of at least 5%, and a glass transition temperature of at least 180 Degrees Fahrenheit. Increased tube strength can also be obtained by forming a layer having at least 80%, by fiber volume, of the fibers

helically oriented relative to the longitudinal axis of the tube at an angle between 30 and 70 degrees.

In accordance with further aspects of the invention, the composite tube includes a liner that serves as a pressure containment member to resist leakage of internal fluids from within the tubing. The inner liner is formed of co-extruded composite polymers. The polymers forming the liner can also include homo-polymers or co-polymers. The polymeric material forming the liner are impermeable to fluids (i.e. gasses and liquids). The inner liner can also include materials that are chemically resistive to corrosives.

The liner can be constructed to have improved mechanical properties that enhance the bending characteristics, the strength characteristics, and the pressure characteristics of the coiled composite tube. For example, the liner can have a mechanical elongation of at least 25%, and a melt temperature of at least 250 degrees Fahrenheit. The liner can also enhance the pressure characteristics of the composite tube by increasing the bonding strength between the inner liner and the composite layer. This can be achieved by placing grooves on the exterior surface of the liner, such that the grooves can hold matrix material that binds the composite layer to the exterior of the liner.

Another feature of the invention includes providing a liner capable of dissipating static charge buildup. A liner having an additive of carbon black can prevent static charge buildup. By preventing static charge buildup, the liner is more likely to prevent the ignition of flammable fluid circulating within the tube.

In a preferred embodiment, the composite layer is formed of three or more fibers interwoven in a triaxial braid and suspended in a matrix material. For example, the composite layer can comprise a helically extending first fiber, a second fiber clockwise extending and helically oriented, and a third fiber counter clockwise extending and helically oriented. The first, second and third fibers are oriented such that the first fiber is interwoven with either the second fiber or the third fiber or both. The composite layer can also include additional plies formed of fiber and matrix. The fibers in the additional plies can have fibers oriented in many ways, including but not limited to, triaxially braiding, biaxially braiding, interwoven and filament wound.

Additional aspects of the invention provide for a separate interface layer interposed between the liner and the composite layer. This interface layer allows the composite coiled tube to withstand extreme pressures inside and outside the tube without causing degradation of the composite tube. The interface layer bonds the composite layer to the liner. In addition, the interface layer can serve as a transition layer between the composite layer and the liner. For example, the interface layer can have a modulus of elasticity between the axial modulus of elasticity of the liner and the axial modulus of elasticity of the composite layer, thereby providing a smooth transition in the modulus of elasticity between the liner and the composite layer.

Other aspects of the invention include a composite coiled tube having a pressure barrier layer. The pressure barrier layer can be located external to the composite layer for preventing fluids (i.e. gases or liquids) from penetrating into the composite tube. The pressure barrier layer also prevents external pressure from being directly applied to the outer surface of the inner liner, thereby preventing exterior pressure from collapsing the inner liner. The pressure barrier layer can be formed of an impermeable material such as either polymeric film (including polyester), thermoplastic, thermoset film, elastomer or metallic film. The impermeable material can be helically or circumferentially wrapped around the composite layer. In addition, the pressure barrier layer can include a fused particle coating. Preferably, the pressure barrier layer has a minimal tensile elongation of 10% and an axial modulus of elasticity of less than 750,000 psi, to aid in the enhanced bending and pressure characteristics of the composite coiled tube.

Further features of the invention provide for a composite tube having an outer protective layer external to the composite layer. The outer protective layer can provide an outer protective surface and an outer wear resistant surface. The outer protective layer can also resist impacts and abrasion. In those aspects of the invention having both a pressure barrier layer and a outer protective layer, the pressure barrier layer is typically sandwiched between the composite layer and the outer protective layer.

Additionally, energy conductors including electrical wiring or fiber optics may be formed as an integral part of the spoolable composite tube. Energy conductors commonly have low strain capability and thus can be damaged easily by large deformations such as those imposed by bending. These energy conductors are thus oriented in a helical direction relative to the longitudinal axis of the tube. This orientation minimizes the strain on the energy conductor when the tube bends. In another embodiment, energy conductors can be embedded in an axial or helical orientation directly into the polymeric liner.

Various embodiments of the invention exist which include one or more aspects and features of the invention described above. In one embodiment, the spoolable composite tube comprises an inner liner and an outer composite layer. In all embodiments, the tube can be designed to include or exclude an interface layer sandwiched between the inner liner and the composite layer. The interface layer increases the bonding strength between the liner and the composite layer. Other embodiments provide for a composite tube including a liner, a composite layer, and a pressure barrier. Further embodiments include a liner, a composite layer, a pressure barrier, and an external protective layer. While in an additional embodiment, the composite tube might include only a liner, a composite layer, and a pressure barrier. The invention also contemplates a spoolable tube having a liner, an inner composite layer, a pressure barrier, and an outer composite layer surrounding the pressure barrier.

**Brief Description of the Drawings**

A more complete understanding of the invention may be obtained by reference to the drawings in which:

FIGURE 1 is a side view, partially broken away, of a composite coiled tube  
5 constructed according to the invention that includes a liner and a composite layer;

FIGURE 2 is a side view of a flattened out composite layer, constructed according to the invention, that has triaxially braided fiber components and which is suitable for constructing the composite layer of the composite tube shown in FIGURE 1;

FIGURE 3 is a cross-sectional view of the composite coiled tube having an  
10 inner liner surrounded by multiple composite layers;

FIGURE 4 is a side view, partially broken away, of a composite coiled tube constructed according to the invention having a liner, an interface layer, and a composite layer;

FIGURE 5 is a side view, partially broken away, of a composite coiled tube  
15 constructed according to the invention having a liner, an interface layer, a composite layer, and a pressure barrier;

FIGURE 6 is a side view, partially broken away, of a composite coiled tube constructed according to the invention that includes a liner, an interface layer, a composite layer, a pressure barrier, and an outer protective layer;

20 FIGURE 7 is a side view, partially broken away, of a composite coiled tube constructed according to the invention that includes a liner, a composite layer, and a pressure barrier;

FIGURE 8 is a side view, partially broken away, of a composite coiled tube  
25 constructed according to the invention comprising a liner, an inner composite layer, a pressure barrier, and an outer composite layer;

FIGURE 9 is a side view, partially broken away, of a composite coiled tube constructed according to the invention that includes an energy conductor; and

FIGURE 10 illustrates the bending events that occur when running coiled tubing in and out of a well bore.

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**Detailed Description of Illustrated Embodiments**

Composite fibers (graphite, Kevlar, fiberglass, boron, etc.) have numerous assets including high strength, high stiffness, light-weight, etc.. however, the stress strain response of composite fibers is linear to failure and therefore non ductile. Composite coiled tubing must therefore address the strain limitations in another manner, i.e., by providing a construction to meet the requirements with a near elastic response or with large deformations of the matrix. Such a composite arrangement must have high resistance to bending stresses and internal pressure and external pressure. It must also have high axial stiffness, high tensile and compressive strength and be resistant to shear stress. All of these

properties are combined in the composite tubular member of the invention to provide a coiled tubing which can be bent to a radius compatible with winding onto a reasonable size spool.

P.K. Mallick in the text book entitled Fiber-Reinforced Composites,

- 5    Materials, manufacturing and Design, defines a composite in the following manner:  
"Fiber-reinforced composite materials consist of fibers of high strength and modulus  
embedded in or bonded to a matrix with distinct interfaces (boundary) between them. In  
general, fibers are the principal load-carrying member, while the surrounding matrix keeps  
them in the desired location and orientation, acts as a load transfer medium between them,  
10 and protects them from environmental damages due to elevated temperatures and humidity,  
for example". This definition defines composites as used in this invention with the fibers  
selected from a variety of available materials including carbon, aramid, and glass and the  
matrix or resin selected from a variety of available materials including thermoset resin such  
as epoxy and vinyl ester or thermoplastic resins such as polyetheretherketone (PEEK),  
15 polyetherketoneketone (PEKK), nylon, etc. Composite structures are capable of carrying a  
variety of loads in combination or independently, including tension, compression, pressure,  
bending, and torsion.

- Webster's Ninth New Collegiate Dictionary defines hose as "a flexible tube  
for conveying fluids". By comparison, a hose is distinctly different from a composite tube.  
20 Hose products such as umbilical lines used in subsea application are constructed of high  
strength fibers such as aramid, dacron, or nylon laid down in a geodesic pattern onto a  
substrate plastic liner tubular structure. Alternatively, a hose may be constructed of high  
strength fibers with a low modulus binder such as rubber. In either case, a hose is designed  
to carry pressure loads and to exhibit good bending flexibility, but a hose has very limited  
25 ability to carry compressive, tension and torsion loads or external pressure.

- The composite tube described in this invention cannot only carry high  
internal pressure but can also carry high compressive, tension and torsion loads,  
independently or in combination. Such capability is essential if the tubing is to be used for  
applications such as coiled tubing in which the tubing is pushed into a high pressure  
30 reservoir and to overcome the friction to movement within the well bore, especially for  
highly deviated or horizontal wells. In addition, the tube is required to carry its own weight  
as it is suspended for 20,000-feet or more in a well bore and to be able to have high pulling  
capability to extract tools or to overcome being struck from sand and circulating solids  
which have collapsed around the tube. Such loads in the case of coiled tubing in deep wells  
35 can be in excess of 20,000 pounds. In other applications the tubing must also be capable of  
carrying high torsion loads. It was not considered feasible until the development  
represented in the current patent application, that one could design and build a composite  
tube capable of being bent to a relatively small diameter such as required for coiled tubing  
spooling and simultaneously be capable of carrying internal pressure and other loads.

In forming composite structures, several well known techniques may be used such as pultrusion, fiber winding, braiding and molding. In pultrusion, fibers are drawn through a resin impregnating apparatus, then through dies to provide the desired shape. Alternatively, the resin may be injected directly within the die. Heat forming and curing structures are provided in conjunction with the dies. In fiber winding, the various layers forming the composite structure are each formed by winding or wrapping fibers and a polymer matrix around a mandrel or some other underlying structure that provide a desired shape. Successive composite layers can then be applied to underlying composite layers. A triaxial braiding structure can be manufactured using the fiber winding techniques disclosed in Quigley, U.S. Patent No. 5,188,872 and in Quigley, U.S. Patent No. RE 35,081.

FIGURE 1 illustrates a composite coiled tube 10 constructed of an inner liner 12 and a composite layer 14. The composite coiled tube is generally formed as a member elongated along axis 17. The coiled tube can have a variety of tubular cross-sectional shapes, including circular, oval, rectangular, square, polygonal and the like. The illustrated tube has a substantially circular cross-section.

Liner 12 serves as a pressure containment member to resist leakage of internal fluids from within the composite coiled tube 10. In one embodiment the liner 12 is metallic, and in an alternative embodiment the liner 12 is formed of polymeric materials having an axial modulus of elasticity exceeding 100,000 psi. A liner having a modulus exceeding 100,000 psi is preferable as it is indicative of a tube capable of carrying high axial tension that does not cause the tube to compress or break. In addition, a liner with an axial modulus of elasticity less than 500,000 psi advantageously allows the liner to bend, rather than pull away from the composite layer, as the composite tube is spooled or bent around a reel.

The polymeric materials making up the liner 12 can be thermoplastic or thermoset materials, for instance the liner can be formed of homo-polymers, co-polymers, composite polymers, or co-extruded composite polymers. Homo-polymers refer to materials formed from a single polymer, co-polymers refers to materials formed by blending two or more polymers, and composite polymers refer to materials formed of two or more discrete polymer layers that have been permanently bonded or fused. The polymeric materials forming the inner liner are preferably selected from a group of various polymers, including but not limited to: polyvinylidene fluoride, ethylene tetrafluoroethylene, cross-linked polyethylene ("PEX"), polyethylene, and polyester. Further exemplary thermoplastic polymers include materials such as polyphenylene sulfide, polyethersulfone, polyethylene terephthalate, polyamide, polypropylene, and acetyl.

Liner 12 can also include fibers to increase the load carrying strength of the liner and the overall load carrying strength of the spoolable composite tube 10. Exemplary

composite fibers include graphite, kevlar, fiberglass, boron, and polyester fibers, and aramid.

The liner 12 can be formed to be resistive to corrosive chemicals such as heterocyclic amines, inorganic sulfur compound, and nitrogenous and acetylenic organic compounds. Three types of liner material, polyvinylidene fluoride ("PVDF"), ethylene tetrafluoroethylene ("ETFE"), and polyethylene ("PE"), have been found to meet the severe chemical exposure characteristics demanded in particular applications involving composite coiled tubing. Two particularly attractive materials for the liner are the RC10-089 grade of PVDF, manufactured by Atochem, and Tefzel® manufactured DuPont.

In other embodiments of liner 12, the liner comprises co-polymers formed to achieve enhanced liner characteristics, such as corrosion resistance, wear resistance and electrical resistance. For instance, a liner 12 can be formed of a polymer and an additive such that the liner has a high electrical resistance or such that the liner dissipates static charge buildup within the composite tube 10. In particular, carbon black can be added to a polymeric material to form a liner 12 having a resistivity on the order of  $10^8$  ohms/centimeter. Accordingly, the carbon black additive forms a liner 12 having an increased electrical conductivity that provides a static discharge capability. The static discharge capability advantageously prevents the ignition of flammable fluids being circulated within the composite coiled tube 10.

In a further aspect of the invention, the liner 12 has a mechanical elongation of at least 25%. A liner with a mechanical elongation of at least 25% can withstand the increased bending and stretching strains placed upon the liner as it is coiled onto a reel and inserted into and removed from various well bores. Accordingly, the mechanical elongation characteristics of the liner prolong the overall life of the composite coiled tube 10. In addition, the liner 12 preferably has a melt temperature of at least 250° Fahrenheit so that the liner is not altered or changed during the manufacturing process for forming the composite coiled tubing. A liner having these characteristics typically has a radial thickness in the range of 0.02 - 0.25 inches.

The composite layer 14 can be formed of a number of plies, each ply having fibers disposed with a matrix, such as a polymer, resin, or thermoplastic. The fibers typically comprise structural fibers and flexible yarn components. The structural fibers are formed of either carbon, nylon, polyester, aramid, thermoplastic, or glass. The flexible yarn components, or braiding fibers, are formed of either nylon, polyester, aramid, thermoplastic, or glass. The fibers included in layer 14 can be woven, braided, knitted, stitched, circumferentially wound, or helically wound. In particular, the fibers can be biaxially or triaxially braided. The composite layer 14 can be formed through pultrusion processes, braiding processes, or continuous filament winding processes. A tube formed of the liner 12 and the composite layer 14 form a composite tube having a maximum tensile

strain of at least 0.25 percent and being capable of maintaining an open bore configuration while being spooled on a reel.

The liner 12, illustrated in FIG. 1, can also include grooves 15 or channels on the exterior surface of the liner. The grooves increase the bonding strength between the liner 12 and the composite layer 14 by supplying a roughened surface for the fibers in the composite layer 14 to latch onto. The grooves can further increase the bonding strength between the liner 12 and the composite layer 14 if the grooves are filled with a matrix. The matrix acts as a glue, causing the composite layer to be securely adhered to the underlying liner 12. Preferably, the grooves are helically oriented on the liner relative to the longitudinal axis 17.

FIGURE 2 shows a "flattened out" view of a preferred composite layer 14 having a fiber component 20 interwoven with a plurality of like or different fiber components, here shown as a clockwise helically oriented fiber component 16 and a counterclockwise helically oriented fiber component 18. The configuration of layer 14 shown in FIGURE 2, is appropriately denoted as a "triaxially braided" ply. The fiber components 16, 18, 20 are suspended in a matrix 22.

Helically oriented fibers are fibers that follow a spiral path. Typically, helical fibers spiral around a mandrel underlying the composite tube or they spiral around underlying layers of the composite tube. For example, a helically oriented fiber follows a path comparable to the grooves around the shaft of a common screw. A helical fiber can be described as having an axial vector, an angle of orientation, and a wrapping direction. The axial vector indicates that the helical fiber can follow a path along the length of the tube 10 as it spirals around the tube, as opposed to a fiber that continually wraps around a particular section of the tube 10 without extending along the length of the tube. The angle of orientation of the helical fiber indicates the helical fiber's angle relative to a defined axis, such as the longitudinal axis 17. For example, a helical fiber having an angle of 0 degrees is a fiber that extends parallel to the longitudinal axis and that does not wrap around the tube 10, while a fiber having an angle of 90 degrees circumferentially wraps around the tube 10 without extending along the length of the tube. The wrapping direction of the helical fiber is described as either clockwise or counter-clockwise wrapping around the tube 10.

The fiber components can be formed of carbon, glass, aramid (such as kevlar® or twaron®), thermoplastic, nylon, or polyester. Preferably, fibers 16 and 18 act as braiding fibers and are formed of either nylon, polyester, aramid, thermoplastic, or glass. Fiber 20 acts as a structural fiber and is formed of either carbon, glass, or aramid. Fiber 20 increases the axial strength of the composite layer 14 and the spoolable tube 10.

The matrix material 22 is generally a high elongation, high strength, impact resistant polymeric material such as epoxy. Other alternative matrixes include nylon-6,

vinyl ester, polyester, polyetherketone, polyphenylene sulfide, polyethylene, polypropylene, and thermoplastic urethanes.

Fiber 20 extends helically or substantially axially relative to the longitudinal axis 17. The helically oriented fiber component 16 and 18 tend to tightly bind the longitudinal fiber component 20 with the matrix material 22 in addition to providing increased bending stiffness along axis 17 and increased torsional strength around axis 17. The helically oriented fiber components 16 and 18 can be interwoven amongst themselves. To this end, successive crossings of two fiber components 16 and 18 have successive "over" and "under" geometries.

According to a preferred aspect of the invention, the composite layer includes a triaxial braid that comprises an axially extending fiber component 20, a clockwise extending second fiber component 16 and a counter-clockwise extending third fiber component 18, wherein the fiber 20 is interwoven with either fiber 16 or fiber 18. Each helically oriented fiber 16, 18 can therefore be considered a braiding fiber. In certain aspects of the invention, a single braiding fiber, such as fiber 16 binds the fiber component of a given ply together by interweaving the braiding fiber 16 with itself and with the axially extending fiber 20. A fiber is interwoven with itself, for example, by successively wrapping the fiber about the member and looping the fiber with itself at each wrap.

In another aspect of the invention, axially extending structural fiber 20 is oriented relative to the longitudinal axis 17 at a first angle 28. Typically, fiber 20 is helically oriented at the first angle 28 relative to the longitudinal axis 17. The first angle 28 can vary between 5° - 20°, relative to the axis. The first angle 28 can also vary between 30° - 70°, relative to the axis 17. Although it is preferred to have fiber 20 oriented at an angle of 45° relative to axis 17.

The braiding fiber 16 is oriented relative to structural fiber 20 at a second angle 24, and braiding fiber 18 is oriented relative to structural fiber 20 at a third angle 26. The angle of braiding fibers 16 and 18, relative to structural fiber 20, may be varied between +\/- 10° and +\/- 60°. In one aspect of the invention, fibers 16 and 18 are oriented at an angle of +\/- 20° relative to fiber 20.

One failure mechanism of the composite tube during loading, especially under bending/pressure and tension and compression loading, is believed to be the development of micro-cracks in the resin and the introduction of microscopic defects between fibers. The development of some micro-cracks is also believed to be inevitable due to the severe loads placed on the tube during the manufacturing and bending of the tube. However, the effects of these micro-cracks and microscopic defects can be retarded by restraining the growth and accumulation of the micro-cracks and microscopic defects during the manufacturing and use of the composite coiled tube. The applicants have discovered that the selection of fibers 16 and 18 from the group of fibers consisting of nylon, polyester, glass and aramid mitigates and stops the growth of the microscopic

defects. Thus, the selection of fibers 16 and 18 from the particularly noted materials improves the damage tolerance and fatigue life of the composite coiled tubing 10.

Applicant has further determined that the total volume of any particular fibrous material in any selected layer of the composite coiled tube affects the overall mechanical characteristics of the composite coiled tube 10, including a reduction in crack propagation. It additionally follows that the total volume of any particular fibrous material in the whole composite coiled tube also affects the mechanical characteristics of the composite coiled tube 10. A composite coiled tube having improved strength and durability characteristics is obtained by forming a composite layer 14 wherein the combined fiber volume of the clockwise extending and counter-clockwise extending braiding fibers 16 and 18 constitute less than 20% of the total fiber volume in the composite layer 14. Further in accordance with this embodiment, the fiber volume of the axially extending fiber 20 should constitute at least 80% of the fiber volume of the composite layer 14. Preferably, the first composite layer 14 includes at least 80% by fiber volume of substantially continuous fibers oriented relative to the longitudinal axis 17 of the tube at an angle between 30-70 degrees.

When the matrix 20 is added to composite layer 14, the volume of matrix in the layer 14 typically accounts for 35% or more of the volume in the composite layer 14. Accordingly, the combined volume of all the fibers in composite layer 14 account for less than 65% of the volume of the composite layer 14. It is thus evident, that the volume of fibers 16 and 18 account for less than 13% of the total volume of the composite layer 14 and that the volume of fiber 20 accounts for at least 52% of the total volume of the composite layer 14.

Matrix 20 in composite layer 14 is selected such that transverse shear strains in the laminar can be accommodated without breaching the integrity of the coil composite tube 10. The strains generally is the result of bending the spoolable composite tube over the reel. These strains do not impose significant axial stresses on the fiber, but they do impose significant stresses on the matrix 20. Accordingly, matrix 20 should be chosen such that the maximal tensile elongation is greater than or equal to 5%. The Applicant has further shown that choosing a matrix having a tensile modulus of at least 100,000 psi adds to the ability of the coil composite tube to withstand excessive strain due to bending. In accordance with the further aspect of the invention, the matrix 20 also has a glass transition temperature of at least 180° Fahrenheit so that the characteristics of the resin are not altered during high temperature uses involving the coiled composite tube 10. The tensile modulus rating and the tensile elongation ratings are generally measured as the coil composite tube is being manufactured at 70° Fahrenheit. Matrix materials having these characteristics include epoxy, vinyl ester, polyester, urethanes, phenolics, thermoplastics such as nylon, polypropylene, and PEEK.

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FIGURE 3 illustrates a coiled composite tube 10 having an inner liner 12 and a first composite layer 14A, a second composite layer 14B, and a third composite layer 14C. Each of the composite layers is formed of fibers embedded in a matrix, and each of the composite layers successively encompasses and surrounds the underlying composite layer or liner 12. At least one of the composite layers, 14A, 14B, 14C, includes a helically oriented fiber in a matrix. Preferably, at least one of the composite layers 14A, 14B, 14C, contains a ply as described in FIG. 2. In particular, one of the composite layers 14A, 14B, 14C, has a first helically extending fiber, a second clockwise extending fiber, and a third counterclockwise extending fiber wherein the first fiber is interwoven with at least one of the second and third fibers. The other two composite layers contain fiber suspended in a matrix. The fibers can be axially extending, circumferentially wrapped, or helically wrapped, biaxially braided or triaxially braided.

According to one aspect of the invention, the fibers in each of the composite layers are all selected from the same material. In other aspects of the invention, the fibers in each of the composite layers are all selected from different materials. For example, composite layer 14A can comprise a triaxially braided ply having clockwise and counter-clockwise helically oriented fibers formed of polyester and having a helically extending fiber formed of glass; composite layer 14B can comprise a ply having a circumferentially wound kevlar fiber; and composite layer 14C can comprise a triaxially braided ply having a clockwise and counter-clockwise helically oriented fibers formed of glass and having a helically extending fiber formed of carbon.

The Applicant's have discovered that additional composite layers, beyond the initial composite layer 14 of FIG. 1, enhance the capabilities of the coiled composite tube. In particular, the interaction between the additional composite layers creates a synergistic effect not found in a single composite layer. The Applicant discovered that composite layers having carbon fibers carry proportionately more of the load as the strain in the coiled composite tube 10 increases, as compared to an equivalent design using glass fibers or aramid fibers. While a composite layer using kevlar (i.e. aramid) fibers provide excellent pressure/cyclical bending capabilities to the coiled composite tube 10. The kevlar fibers appear to have a weakness when compared to the carbon fibers in compressive strength. Accordingly, a coiled composite tube 10 incorporating both kevlar and carbon fibers provides a composite structure having improved characteristics not found in composite structures having composite layers formed of only carbon fibers or only kevlar fibers.

Accordingly, one aspect of the invention incorporates a composite layer 14A formed of carbon fibers and polyester fibers in a triaxially braided structure and a second composite layer 14B formed of kevlar fibers. The kevlar fibers can be incorporated into either a conventional bi-axial braid, triaxial braid, or helical braid. For instance, the second composite layer can include two sets of aramid fibers bi-axially braided together. The

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coiled composite tube 10 having an inner composite layer 14A formed with carbon fibers and an exterior composite layer 14B formed with kevlar fibers provides a coiled composite tube having balanced strength in two directions and provides a coiled composite tube having a constricting force which helps restrain the local buckling of delaminated sublamina and subsequent delamination growth, thereby improving the fatigue resistance of the coiled composite tube 10. Certainly, this aspect of the invention can include a third composite layer 14C external to the second composite layer 14B. The third composite layer 14C can, for instance, include a matrix and a fiber helically oriented relative to the longitudinal axis 17.

In another aspect of the invention, as illustrated in FIGURE 3, the composite layer 14A comprises a triaxially braided ply having an axially extending fiber formed of carbon and having a clockwise extending fiber and a counter-clockwise extending fiber both formed of polyester. In addition, the helically extending fiber 20 is oriented at an 45° angle to the axis of the coiled composite tube 10. Further in accordance with this embodiment, composite layer 14B is triaxially braided and comprises a helically extending fiber formed of carbon and oriented at an angle of 45° relative to the axis 17 of coiled composite tube 10. Composite layer 14B further includes a clockwise extending second fiber and a counter-clockwise extending third fiber formed of polyester. The third composite layer 14C, is biaxially braided, and comprises a kevlar fiber extending helically and oriented at a 54° angle to the axis 17 of the composite coiled tube 10.

FIGURE 4 illustrates a composite coiled tube elongated along an axis 17 and having an inner liner 12, an interface layer 56, and a composite layer 14. The interface layer 56 surrounds the liner 12 and is sandwiched between the liner 12 and the composite layer 14. The interface layer 56 improves the bonding between the inner liner 12 and the composite layer 14.

It is important in the composite coiled tubing 10 that the liner 12 be integrally attached to the composite layer 14. The necessity for a bonded liner is that in certain operating conditions experienced in down hole service, the external surface of the tube will be subjected to higher pressure than the interior of the tube. If the liner is not bonded to the composite layer 14 this external pressure could force the liner to buckle and separate from the composite layer such that the liner collapses. In addition, loading and bending of the tube may introduce microscopic cracks in the composite layer 14 which could serve as microscopic conduits for the introduction of external pressure to be applied directly to the outer surface of the liner 12. Once again, these external pressures could cause the liner 12 to collapse. The interface layer 56 provides a mechanism for bonding the liner 12 to the composite layer 14 such that the liner does not collapse under high external pressures. The interface layer 56 can also reduce cracking and the propagation of cracking along the composite layer 14 and liner 12.

- In accordance with one aspect of the invention, the interface layer 56 comprises a fiber reinforced matrix where the fiber volume is less than 40% of the total volume of the interface layer 56. The matrix and the fiber forming interface layer 56 predominately act as an adhesive layer that bonds the liner 12 to the composite layer 14.
- 5 The fibers within the interface layer 56 can be oriented in various ways, including a woven or non-woven structure. Preferably, the fibers within the interface layer 56 are polyester fibers. An interface layer having this structure is able to prevent the liner from separating from the composite layer even when the differential pressure between the exterior and interior of the tube 10 exceeds 1,000 psi.
- 10 The matrix within the interface layer 56 can comprise a filled polymeric layer or an unfilled polymeric layer. A filled polymeric layer uses a polymeric matrix having additives that modify the properties of the polymeric layer. The additives used in the filled polymeric layer include particulates and fibers. For instance, carbon black powder can be added to the polymeric layer to increase the conductivity of the interface
- 15 layer 56, or chopped glass fibers can be added to the polymeric layer to increase the stiffness of the interface layer 56.

According to a further embodiment of the invention, the interface layer has an axial modulus of elasticity that lies between the modulus of the elasticity of the liner 12 and the modulus of elasticity of the composite layer 14. The interface layer 56 thus has a 20 modulus of elasticity that transitions between the modulus of elasticity of the liner 12 and the composite layer 14. By providing a transitional modulus of elasticity, the interface layer aids in preventing the liner 12 from pulling away from the composite layer 14 during the bending action of the composite coiled tube 10.

The interface layer 56 furthermore increases the fatigue life of the coiled 25 composite tube 10. The structure of the interface layer 56 achieves this by dissipating shear stress applied along the length of the coiled composite tube 10. By dissipating the shear, the interface layer reduces cracking and the propagation of cracks along the composite layer 14.

FIGURE 5 illustrates a composite coiled tube elongated along an axis 17 30 and having an inner liner 12, an interface layer 56, a composite layer 14, and a pressure barrier layer 58. The pressure barrier layer 58 prevents gases or liquids (i.e. fluids) from penetrating into the composite coiled tube 10.

It is important for two reasons that fluids not penetrate into the composite 35 layer 14. First, a fluid that penetrates through the tube 10 to liner 12 can build up to a sufficient level of pressure capable of collapsing the liner 12. Second, a fluid that penetrates the coiled composite tube 10 during exposure in the well bore 36 may outgas when the coil composite tube 10 is returned to atmospheric pressure.

Accordingly, a coiled composite tube 10 can function effectively without a pressure barrier layer 58 under certain conditions. For example, when micro-fractures and

defects in the composite layer 14 do not develop to a size that allows fluids to penetrate the composite layer 14, a pressure barrier layer is not necessary. However, when micro-fractures and passages through the composite layer 14 do allow for the migration of fluids the use of a pressure barrier layer 58 is preferred. As illustrated in FIG. 5, the pressure barrier layer 58 generally is positioned outside of the composite layer 14.

The pressure barrier layer 58 can be formed of a metal, thermoplastic, thermoset films, or an elastomer such as a rubber sheet. All these various materials can function as a pressure barrier because they substantially prevent the diffusion of fluids. Preferable properties of the pressure barrier layer include low permeability to fluids (i.e., gases or liquids), high elongation, and bondability to composite layer 14. It is also preferred that the pressure barrier layer 58 have a maximum tensile elongation of 10% and an axial modulus of elasticity of less than 750,000 psi. These values of tensile elongation and modulus of elasticity are measured at 70° Fahrenheit during the manufacturing of the coiled composite tube 10. The permeability of the pressure barrier layer should be less than  $0.4 \times 10^{-10}$  ccs per sec-cm<sup>2</sup>-cm-cmhg.

The impermeable pressure barrier layer 58 can be formed of an impermeable films formed of metals or polymers. For instance, acceptable polymeric films include films formed of polyester, polyimide, polyamide, polyvinyl fluoride, polyvinylidene fluoride, polyethylene, and polypropylene, or other thermoplastics.

The impermeable film of layer 58 can be a seamless polymer layer which is coextruded or formed via a powder deposition process. Alternatively, the impermeable film can be helically wrapped or circumferentially wrapped around the composite layer to form an overlapping and complete barrier. That is, the fiber or material forming the pressure barrier layer must be wrapped in such a fashion that no gaps exist and the pressure barrier layer 58 is sealed.

Another aspect of the invention provides for a pressure barrier layer 58 having a fused particle coating. A fused particle coating is formed by grinding a polymeric material into a very fine powder. The fine powder is then heat-fused onto the other materials forming the pressure barrier layer 58 or onto the underlying composite layer 14.

FIGURE 6 illustrates a composite coiled tube elongated along an axis 17 and having an inner liner 12, an interface layer 56, a composite layer 14, a pressure barrier layer 58 and an outer protective layer 60. The interface layer 56 enhances the bond between the composite layer 14 to the inner liner 12. The pressure barrier layer 58 prevents fluids from penetrating into the composite coiled tube 10. The outer protective layer 60 provides wear resistance, impact resistance, and an interface layer for the coupling for the coiled composite tube 10. The protective layer is positioned such that it surrounds the pressure barrier 58.

Outer protective layer 60 provides abrasion resistance and wear resistance by forming an outer surface to the coil composite tube that has a low co-efficient of friction

thereby causing objects to slip off the coiled composite tube. In addition, the outer protective layer 60 provides a seamless layer for holding the inner layers of the coiled composite tube together. The outer protective layer can be formed of a filled or unfilled polymeric layer. Alternatively, the outer protective layer 60 can be formed of a fiber, such as kevlar or glass, and a matrix. The fibers of the outer protective layer 60 can be woven in a mesh or weave pattern around the inner layers of the coiled composite tube 10, or the fibers can be braided or helically braided around the inner layers of tube 10. In either case, the fibers in the outer protective layer are wrapped helically around the inner layers of the coiled composite tube 10 in order to provide a seamless structure.

It has further been discovered by the Applicant that particles can be added to the outer protective layer to increase the wear resistance of the outer protective layer 60. The particles used can include any of the following, individually or in combination with one another: ceramics, metallics, polymers, silicas, or fluorinated polymers. Adding Teflon® (MP 1300) particles and an aramid powder (PD-T polymer) to the matrix of the outer protective layer 60 has been found to be one effective way to reduce friction and enhance wear resistance.

In the case where the outer protective layer includes fibers, the particles added to the outer protective layer 60 are such that they consist of less than 20% by volume of the matrix. In the case where the outer protective layer does not contain fiber, a particulate such as Teflon® MP 1300 can also be added to the polymeric protective layer. When the outer layer 60 does not include fiber, the particles typically comprise less than 60% by coating volume of the outer wear resistant layer 60.

FIGURE 7 illustrates an embodiment of the composite coiled tube elongated along an axis 17 and having a liner 12, a composite layer 14, and a pressure barrier 58. FIG. 7 is similar to FIG. 5, except that it lacks the interface layer 56. Particularly, the inner liner 12 is positioned internally to the composite layer 14, and the composite layer 14 is positioned internally to the pressure barrier 58. This figure illustrates, among other things, that the interface layer 56 can either be included or removed from all embodiments of the invention, depending upon whether the circumstances require the use of an interface layer to increase the bonding strength between the liner and the composite layer.

FIGURE 8 illustrates another embodiment of a composite coiled tube elongated along an axis 17, the composite tube includes a liner 12, a first composite layer 14, a pressure barrier 58, and a second composite layer 14'. In this embodiment, the first composite layer 14 surrounds the internal liner, and the pressure barrier surrounds the first composite layer 14. In addition, the second composite layer 14' surrounds the pressure barrier 58. Particularly, the pressure barrier is sandwiched between two composite layers 14 and 14'.

Composite layer 14' can be structured in any manner that composite layer 14 can be structured, but the layers 14 and 14' need not be identical. In addition, either

composite layer 14 or composite layer 14' can include multiple composite layers as illustrated in FIG. 3. The external composite layer 14' proves useful in providing an exterior surface capable of engaging a coupling device.

The external composite layer 14' can also be fashioned to act as an outer protective layer capable of providing abrasion resistance and wear resistance. This can be achieved by forming the external composite layer 14' from a filled or unfilled polymeric layer. The layer 14' can also achieve increased abrasion and wear resistance by helically wrapping or braiding those fibers forming composite layer 14' around the inner layers of the tube 10. Furthermore, the external composite layer 14' can be fashioned to reduce the friction of the exterior of tube 10 by adding particles to the external composite layer 14'. The particles can include ceramics, metallics, polymerics, silicas, or fluorinated polymers.

FIGURE 9 illustrates a composite coiled tube elongated along an axis 17 wherein the composite tube includes a liner 12, a composite layer 14, and an energy conductor 60 forming part of the composite layer 14. The energy conductor provides a path for passing power, communication or control signals from the surface down through the tube to a machine attached to the end of the tube.

The energy conductor 60 can be located in either the liner, the composite layers, or the pressure barrier forming the tube 10. But it is preferable to locate the energy conductors in those layers nearest the interior surface of the tube and not in those layers located near the exterior surface of the tube. If an energy conductor is located near the exterior surface of the tube it is more likely to be subjected to corrosive surfaces or materials located outside the tube 10. In addition, an energy conductor located near the interior of the tube 10 will be subjected to smaller bending strains when compared to an energy conductor located near the exterior of the tube.

An energy conductor can be embedded in any of the layers forming the tube 10 using the same methods known in the art for adding a fiber to the composite layer. Typically, an energy conductor is wound onto a mandrel or any underlying structure while applying a matrix. Energy conductors can also be added to a fiber composite layer with a pultrusion process. For example, the energy conductor can be drawn through a resin impregnating apparatus, then through dies to provide the desired shape. Alternatively, the conductor can be embedded in the polymer liner.

The energy conductor 60 may be an electrical or optical conductor of any material or substance capable of being modulated with information data or electrical power. A primary concern in placing the conductor 60 in the inner areas of the composite tube 10 is to ensure that the bending strains on the conductor 60 are minimized. This is particularly critical if the conductor 60 is a fiber optic cable. Moreover, the energy conductor 60 is typically helically oriented relative to the longitudinal axis 17 of the composite tube to minimize the bending strain on conductor 60. The helical orientation allows the compression strain experienced by the section of the conductor located on the interior bend

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of the tube to be offset by the expansion strain experienced by the section of the conductor located on the exterior bend of the tube. That is, the conductor 60 is able to substantially distribute the opposing strains resulting from the bending action of the composite tube across the length of the conductor 60, thereby preventing irreparable damage to the  
5 conductor.

FIGURE 10 illustrates the bending cycles that a coiled composite tube 10 is subjected to when performing a typical coiled tubing service. The tubing 10 is inserted and removed from a well bore 36 located below the ground surface. A reel 42 is provided on the surface and the composite coiled tube 10 is stored on the reel 42. An injector assembly 10 38 is located on the surface over the well bore 36. Injector assembly 38 typically contains a roller belt 40 used to guide the coiled composite tube 10 through the injector assembly 38 into the well bore 36. The coiled composite tube 10 typically is subjected to six bending events as it is inserted and removed from the well bore 36. The first bending event 44 takes place when the coiled composite tube 10 is pulled off the service reel 42. When the coiled 15 composite tube 10 reaches the assembly 38, the coiled tube passes through two bending events 46 and 48. The bending events 50, 52 and 54 are the reverse of bending events 44, 46, 48 and occur as the coiled composite tube 10 is extracted from the well bore 36. The insertion and extraction of the tube 10 thus results in a total of six bending events for every round trip of the coiled composite tube 10. The current steel tubing being used in the field 20 can generally be cycled three times through the bending events described in FIGURE 4 in conjunction with high internal pressures before the steel tubing fails. In comparison, the coiled composite tube of the Applicant's invention can be cycled 10,000 times through the bending events described in FIGURE 4.

It is also to be understood that the following claims are to cover all generic 25 and specific features of the invention described herein, and all statements of the scope of the invention which, as a matter of language, might be said to fall there between.

Having described the invention, what is claimed as new and secured by Letters Patent is:

Claims

1. A spoolable composite tube, said tube comprising
  - 5 an inner liner formed from polymeric materials, said liner being substantially fluid impervious, and a first composite layer enclosing said liner and formed of fiber and matrix, said first composite layer having a first fiber extending helically and having a second clockwise extending fiber and having a third counter clockwise extending fiber, such that
    - 10 said first fiber is interwoven with at least one of said second fiber and said third fiber.
2. A composite tube according to claim 1, wherein said liner has a radial thickness between 0.02 inches and 0.25 inches.
- 15 3. A composite tube according to claim 1, wherein said liner has a mechanical elongation of at least 25% and a melt temperature of at least 250 degrees Fahrenheit.
4. A composite tube according to claim 1 wherein said polymeric materials forming said liner are co-extruded composite polymers.
- 20 5. A composite tube according to claim 4 wherein said polymeric materials forming said liner are selected from the group consisting of polyvinylidene fluoride, ethylene tetrafluoroethylene, cross-linked-polyethylene, polyamide, polyethylene, and polyester.
- 25 6. A composite tube according to claim 1, wherein said liner further comprises ethylene tetrafluoroethylene, such that said liner is chemically resistant to corrosives selected from the group consisting of heterocyclic amines, inorganic sulfur compounds, and nitrogenous and acetylenic organic compounds.
- 30 7. A composite tube according to claim 1, further comprising an interface layer for bonding said first composite layer to said liner, such that said liner withstands separation from said composite layer at a differential pressure between the exterior and interior of said tube of at least 1,000 psi.
- 35 8. An interface layer according to claim 7, wherein said interface layer comprises a fiber reinforced matrix where the fiber volume is less than 40%.

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9. A composite tube according to claim 1, further comprising an interface layer interposed between said liner and said composite layer, said interface layer having a modulus of elasticity between the axial modulus of elasticity of said liner and the axial modulus of elasticity of said composite layer.

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10. A composite tube according to claim 9, wherein said interface layer further comprises a filled polymeric layer.

10. A composite tube according to claim 9, wherein said interface layer further comprises an unfilled polymeric layer.

12. A composite tube according to claim 1, wherein said matrix forming said first composite layer has a tensile modulus of at least 250,000 psi and has a maximum tensile elongation of at least 5% and has a glass transition temperature of at least 180  
15 Degrees Fahrenheit.

13. A composite tube according to claim 1, wherein each of said second fiber and said third fiber is selected from the group consisting of nylon, polyester, thermoplastic, glass, and aramid.

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14. A composite tube according to claim 1, wherein said first fiber is selected from the group consisting of fibers of aramid, carbon, and glass.

15. A composite tube according to claim 1, further comprising a second  
25 composite layer exterior to said first composite layer, said second composite layer being formed from a first set of aramid fibers.

16. A composite tube according to claim 15, further comprising a second set of fibers bi-axially braided with said first set of aramid fibers.

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17. A composite tube according to claim 15, further comprising a second set of aramid fibers woven with said first set of aramid fibers.

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18. A composite tube according to claim 15, further comprising a third composite layer external to said second composite layer, said third composite layer being formed of matrix and a fourth fiber helically oriented relative to the longitudinal axis.

19. A composite tube according to claim 1, wherein said first composite layer includes at least 80% by fiber volume of substantially continuous fibers oriented relative to the longitudinal axis of the tube at an angle between 30 Degrees and 70 Degrees, said substantially continuous fibers having an axial modulus of elasticity in excess of nine million psi.
20. A composite tube according to claim 1 having the further improvement in which the combined fiber volume of said second fiber and said third fiber constitutes less than 20% of the total fiber volume in said first composite layer
21. A composite tube according to claim 1 having the further improvement in which the fiber volume of said first fiber has a volume more than 80% of the fiber volume of said first composite layer.
22. A composite tube according to claim 1, further comprising a pressure barrier layer external to said first composite layer, for preventing fluids from penetrating into said said composite tube.
23. A composite tube according to claim 22, wherein said pressure barrier layer has a minimum tensile elongation of at least 10% and an axial modulus of elasticity of less than 750,000 psi.
24. A composite tube according to claim 22, wherein said pressure barrier layer is an impermeable film.
25. A composite tube according to claim 24, wherein said impermeable film is helically wrapped around said composite layer.
26. A composite tube according to claim 24, wherein said impermeable film is selected from the group consisting of metallics, polyester, polyimide, polyamide, polyvinyl fluoride, polyvinylidene fluoride, polyethelyne, polypropylene, and elastomers.
27. A composite tube according to claim 22, wherein said pressure barrier layer includes a fused particle coating of polymeric material.

28. A composite tube according to claim 1, further comprising an outer protective layer external to said first composite layer, said outer protective layer being structured to provide wear resistance and having an outer surface with a coefficient of friction less than the coefficient of friction of said first composite layer.
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29. A composite tube according to claim 28, wherein said outer protective layer further comprises a composite formed of a fiber and a matrix with a particulate.
- 10 30. A composite tube according to claim 29, wherein said outer protective layer further comprises a composite formed of braided, woven, or knit aramid fibers and a matrix with a particulate.
- 15 31. A composite tube according to claim 29, wherein said particulate is selected from the group consisting of ceramics, metallics, polymerics, silicas, and fluorinated polymers.
- 20 32. A composite tube according to claim 29, wherein said matrix includes less than 20% by matrix volume of said particulate.
33. A composite tube according to claim 28, wherein said outer protective layer is a polymeric coating filled with less than 60% by coating volume with a particulate.
- 25 34. A composite tube according to claim 33, wherein said particulate is selected from the group consisting of ceramics, metallics, polymerics, silicas, and fluorinated polymers.
35. A composite tube according to claim 1, wherein said liner further includes a additive for dissipating static charge buildup within said composite tube.
- 30 36. A composite tube according to claim 1, wherein said additive for dissipating static charge buildup within said composite tube is carbon black.
- 35 37. A composite tube according to claim 1, wherein said liner further includes helical grooves for improved bonding to the said composite layer.

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38. A spoolable composite tube, said tube comprising

an inner liner formed from polymeric materials, said liner being substantially fluid impervious, and

5 a first composite layer enclosing said liner, said first composite layer being formed of a matrix and a first set of fibers having at least 80 percent, by fiber volume, of the fibers helically oriented relative to the longitudinal axis at an angle between 30 degrees and 70 degrees,

10 wherein the maximum tensile strain of said composite tube, formed from said liner and said composite layer, when spooled on a reel is at least 0.25 percent.

39. A composite tube according to claim 38, wherein said liner has a radial thickness between 0.02 inches and 0.25 inches.

15 40. A composite tube according to claim 38 wherein said polymeric materials forming said liner are selected from the group consisting of homo-polymers, co-polymers, and composite polymers.

20 41. A composite tube according to claim 38, wherein said liner further comprises ethylene tetrafluoroethylene, such that said liner is chemically resistant to corrosives selected from the group consisting of heterocyclic amines, inorganic sulfur compounds, and nitrogenous and acetylenic organic compounds.

25 42. A composite tube according to claim 38, further comprising an interface layer for bonding said first composite layer to said liner, such that said liner withstands separation from said composite layer at a differential pressure between the exterior and interior of said tube of at least 1,000 psi.

30 43. A composite tube according to claim 38, further comprising an interface layer interposed between said liner and said composite layer, said interface layer having a modulus of elasticity between the axial modulus of elasticity of said liner and the axial modulus of elasticity of said composite layer.

35 44. A composite tube according to claim 38, wherein said matrix forming said first composite layer has a tensile modulus of at least 250,000 psi and has a maximum tensile elongation of at least 5% and has a glass transition temperature of at least 180 Degrees Fahrenheit.

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45. A composite tube according to claim 38, wherein said first set of fibers further comprises

a set of structural fibers selected from the group consisting of aramid, carbon, and glass, and

5 a set of braiding fibers selected from the group consisting of nylon, polyester, thermoplastic, glass, and aramid.

46. A composite tube according to claim 38, further comprising a second composite layer exterior to said first composite layer, said second composite layer being  
10 formed of a first set of aramid fibers and matrix.

47. A composite tube according to claim 38, said liner further includes at least one embedded energy conductor therein.

15 48. The spoolable composite tube of claim 47 wherein said energy conductor is a metal.

49. The spoolable composite tube of claim 47 wherein said energy conductor extends helically within the said liner.

20 50. The spoolable composite tube of claim 47 wherein said energy conductor is a light guiding medium.

51. A composite tube according to claim 38, said composite layer further  
25 includes at least one embedded energy conductor therein.

52. The spoolable composite tube of claim 51 wherein said energy conductor is a metal.

30 53. The spoolable composite tube of claim 51 wherein said energy conductor extends helically within the said composite layer.

54. The spoolable composite tube of claim 51 wherein said energy conductor is a light guiding medium.

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55. A spoolable composite tube having a longitudinal axis and comprising  
a tubular inner liner formed of polymeric material. said liner being  
substantially fluid impervious,  
a first composite layer enclosing said liner and formed of a helically oriented  
5 first set of fibers and of polymeric matrix,  
an exterior layer external to and enclosing said first composite layer, said  
exterior layer being either a pressure barrier layer formed of an impermeable film or an  
outer protective layer providing wear resistance and having an outer surface with a  
coefficient of friction less than the coefficient of friction of said composite layer, and  
10 wherein said liner and said composite layer and said exterior layer constitute  
a composite tube having a tensile strain of at least 0.25 percent when spooled on a reel, and  
while maintaining an open bore configuration.
56. A composite tube according to claim 55, wherein said impermeable film is  
15 helically wrapped around said composite layer.
57. A composite tube according to claim 55, wherein said impermeable film is  
selected from the group consisting of metallics, polyester, polyimide, polyamide, polyvinyl  
flouride, polyvinylidene fluoride, polyethelyne, polypropylene, and elastomers
- 20
58. A composite tube according to claim 55, wherein said pressure barrier layer  
includes a fused particle coating of polymeric material.
59. A composite tube according to claim 55, wherein said pressure barrier layer  
25 has a minimum tensile elongation of at least 10% and an axial modulus of elasticity of less  
than 750,000 psi.
60. A composite tube according to claim 55, wherein said outer protective layer  
further comprises a composite formed of a fiber and a matrix with a particulate.
- 30
61. A composite tube according to claim 55, wherein said fiber in said outer  
protective layer is aramid.
62. A composite tube according to claim 60, wherein said particulate is selected  
35 from the group consisting of ceramics, metallics, polymers, silicas, and fluorinated  
polymers.

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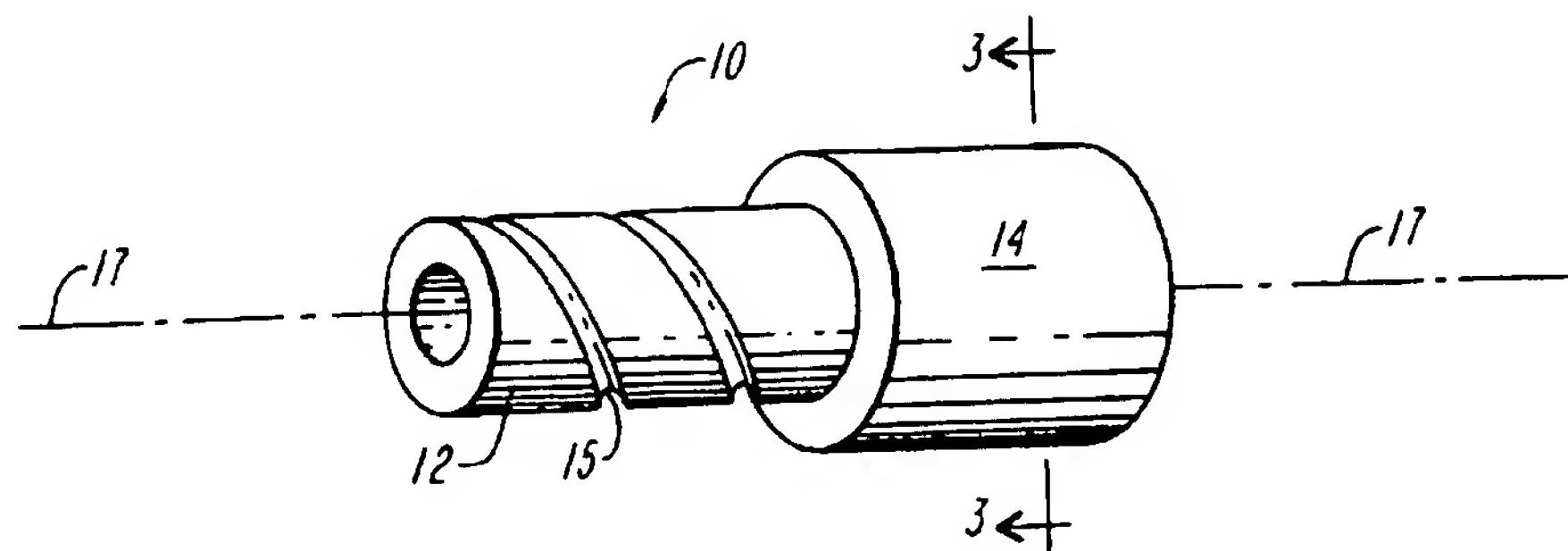


FIG. 1

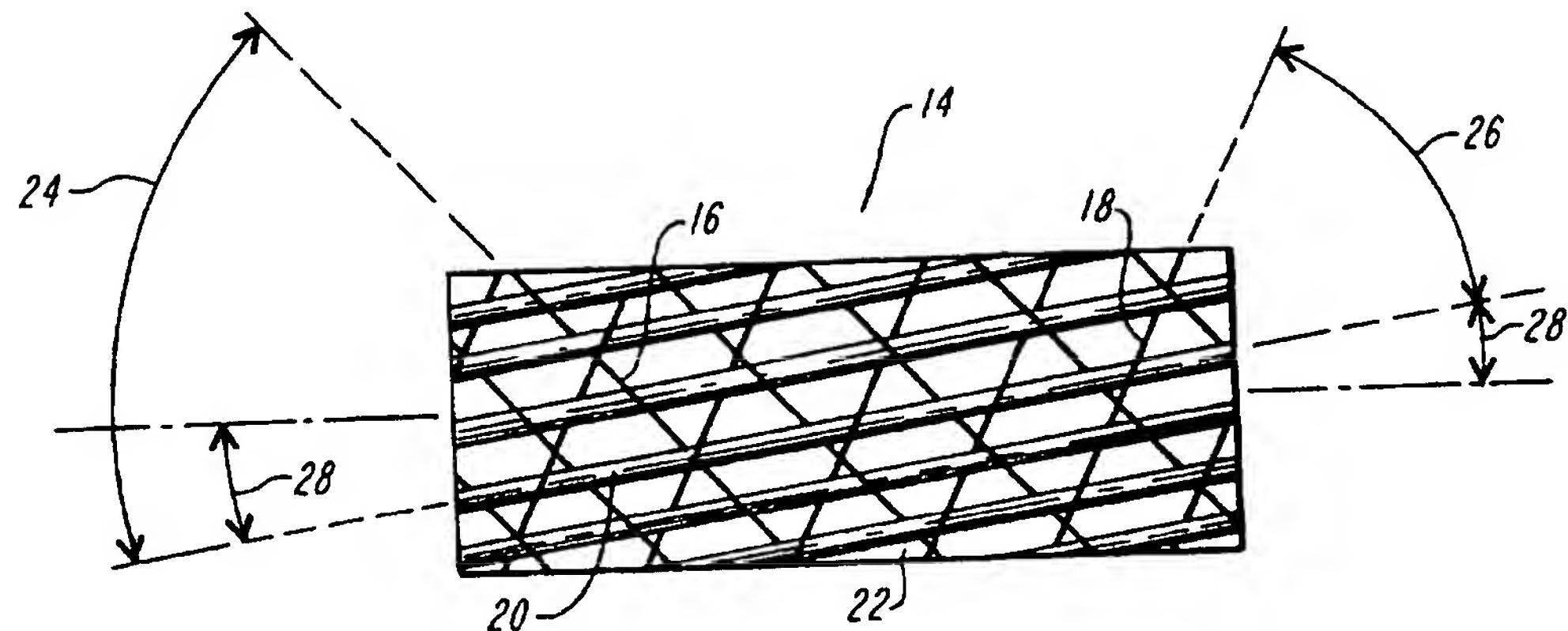


FIG. 2

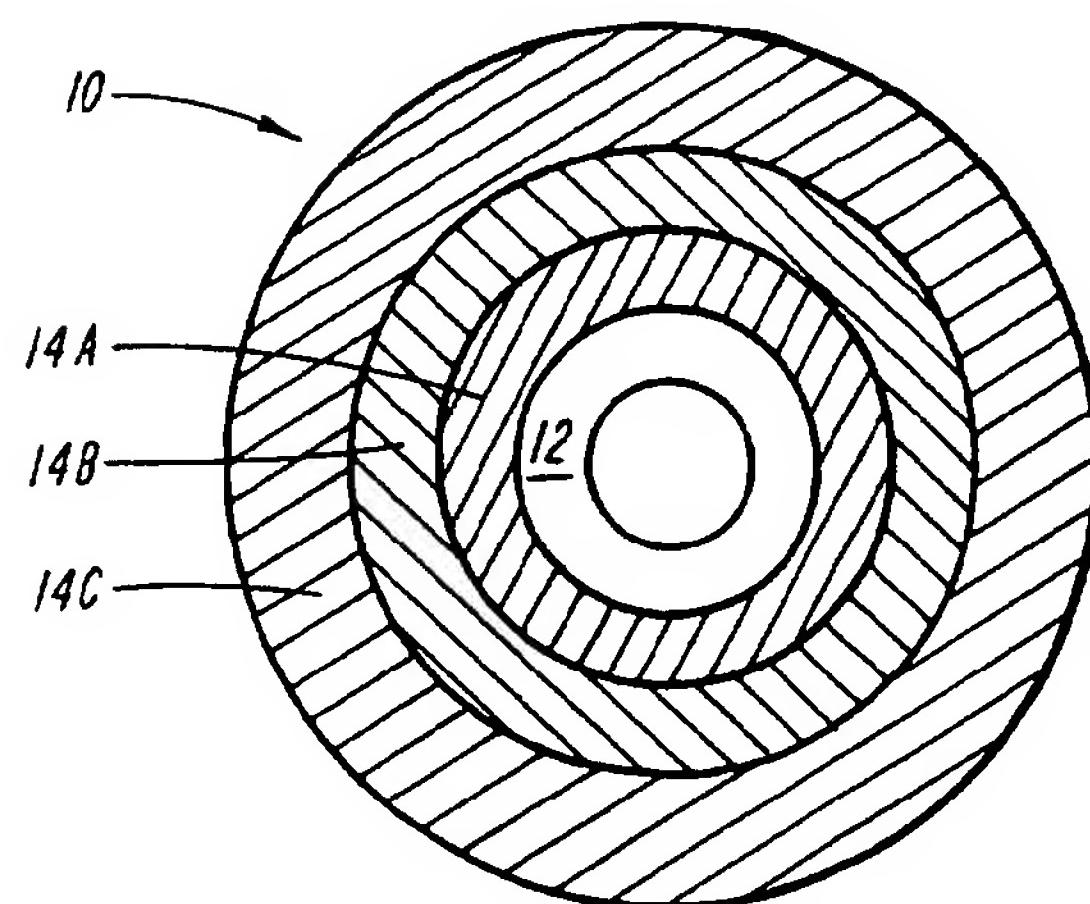


FIG. 3

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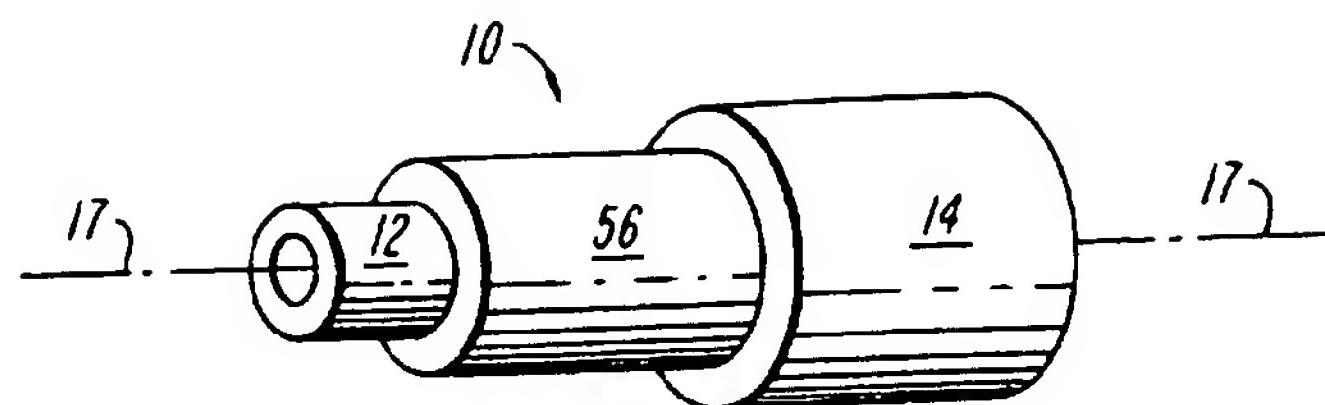


FIG. 4

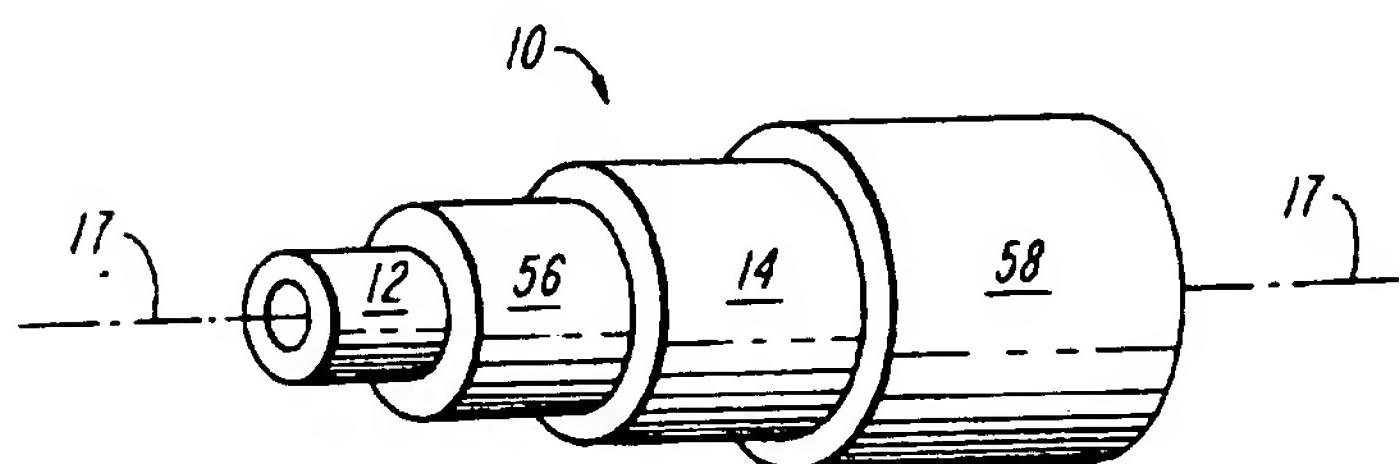


FIG. 5

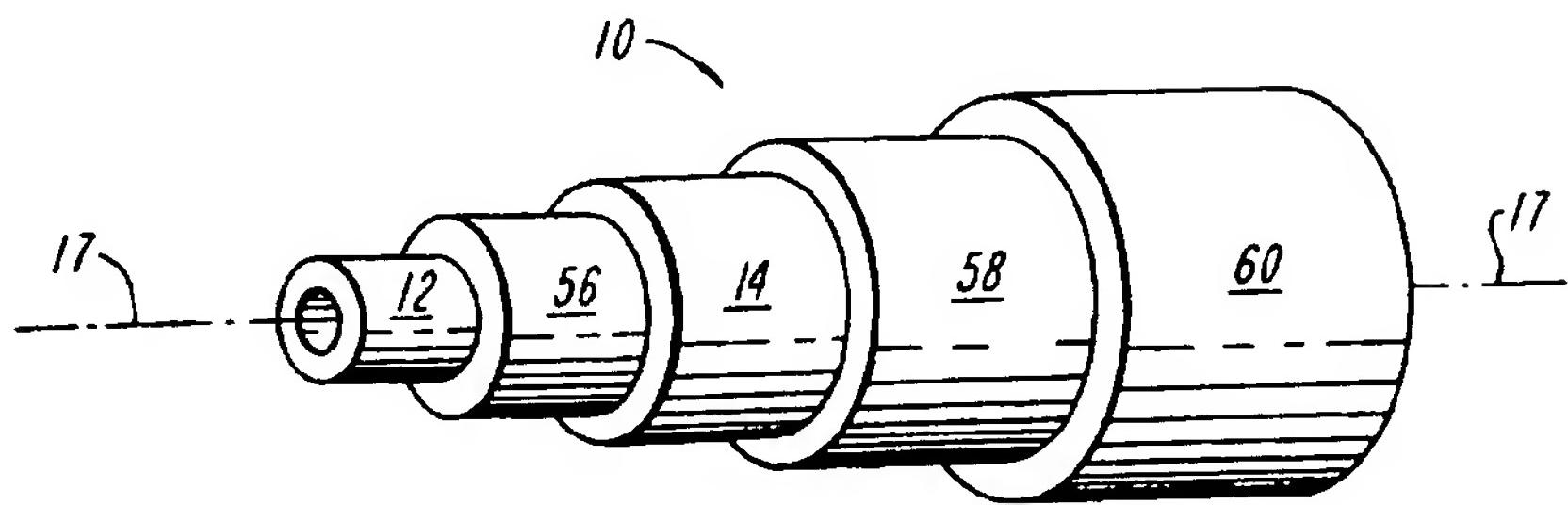


FIG. 6

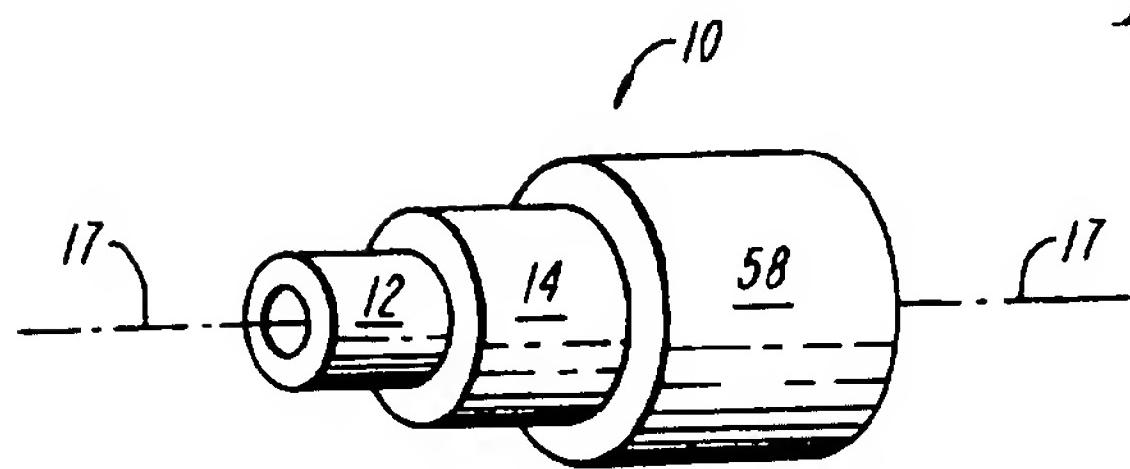
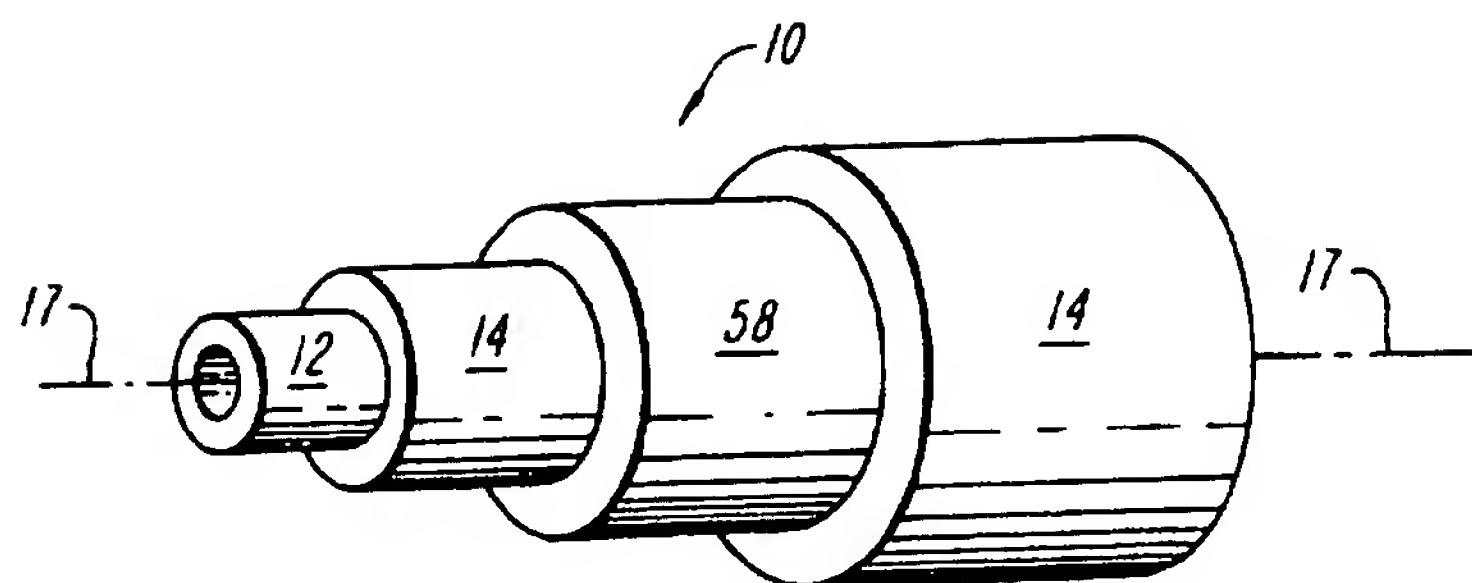


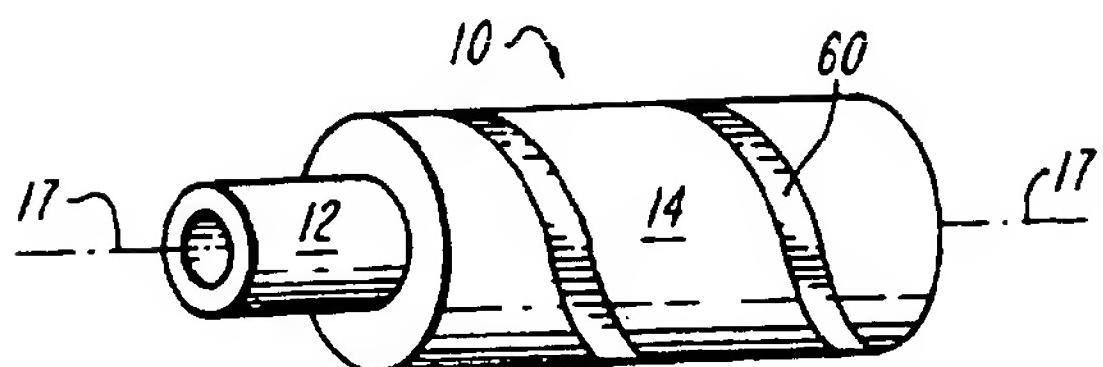
FIG. 7

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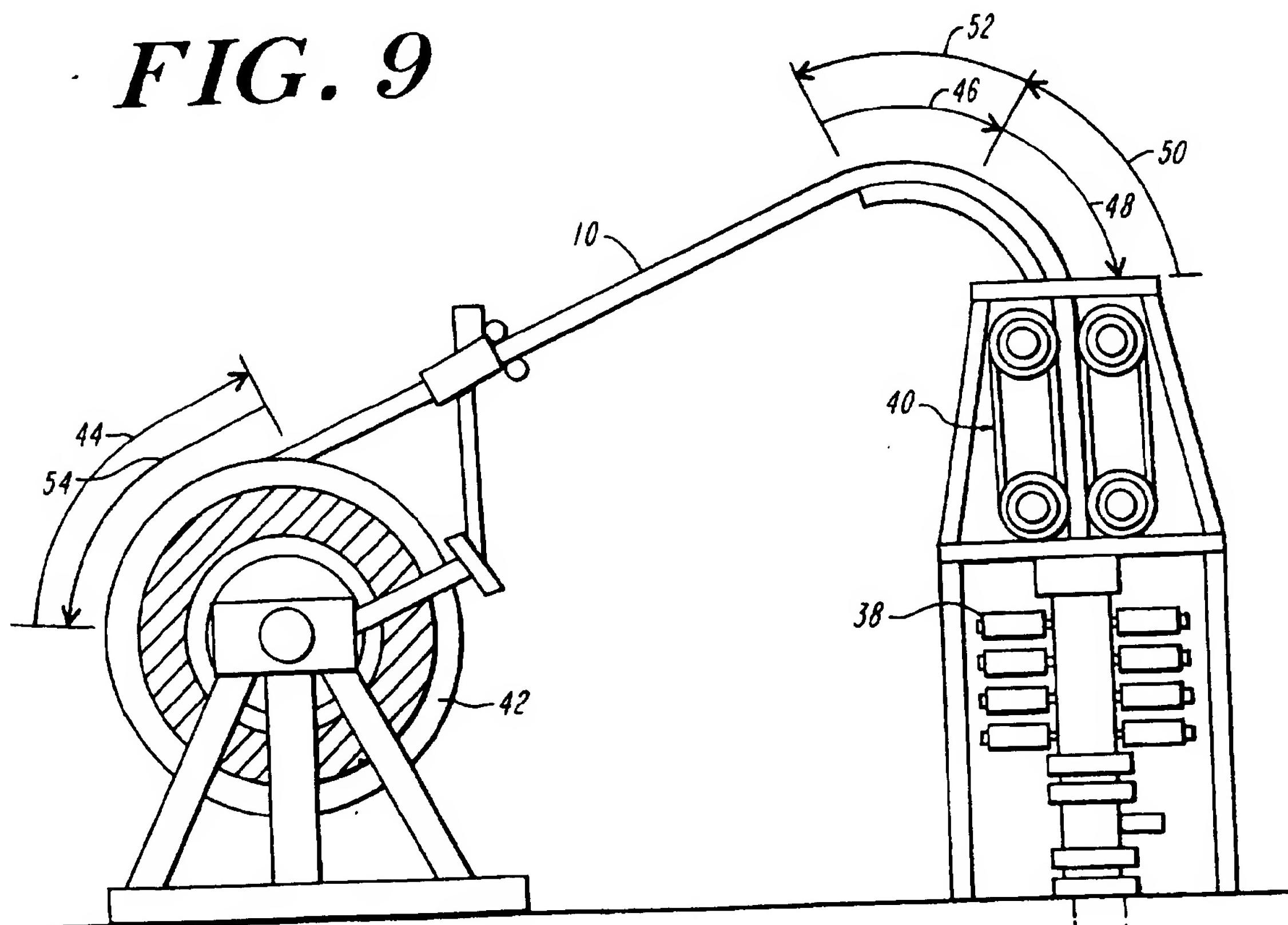
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*FIG. 8*



*FIG. 9*



*FIG. 10*

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# INTERNATIONAL SEARCH REPORT

Inte  
nal Application No  
PCT/US 96/15625

**A. CLASSIFICATION OF SUBJECT MATTER**  
 IPC 6 F16L11/08 F16L11/127

According to International Patent Classification (IPC) or to both national classification and IPC

**B. FIELDS SEARCHED**

Minimum documentation searched (classification system followed by classification symbols)  
 IPC 6 F16L

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

**C. DOCUMENTS CONSIDERED TO BE RELEVANT**

Category	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	US,A,4 303 457 (H. A. JOHANSEN ET AL.) 1 December 1981  see the whole document	1,4-6, 13,28, 29,35,36
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X	US,A,2 810 424 (E. E. SWARTSWELTER ET AL.) 22 October 1957 see the whole document	1,4,5,13
X	US,A,4 261 390 (BELOFSKY) 14 April 1981 see the whole document	1,4,5
A	---	37
		-/-

Further documents are listed in the continuation of box C.

Patent family members are listed in annex.

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1

Date of the actual completion of the international search

Date of mailing of the international search report

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## INTERNATIONAL SEARCH REPORT

Inte:      nal Application No  
PCT/US 96/15625

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A	US,A,3 116 760 (R. A. MATTHEWS) 7 January 1964 see the whole document ---	1,4,5,13
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